



Cobalt Geosciences, LLC  
P.O. Box 1792  
North Bend, WA 98045

September 2, 2025  
Updated October 21, 2025

MacPherson Construction and Design  
Attn: Mr. Dan Buchser  
[dan@macphersonconstruction.com](mailto:dan@macphersonconstruction.com)

**RE: Plan Review & Comment Responses**  
Proposed Additions/Remodel  
5320 Butterworth Road – CAO25--011  
Mercer Island, Washington

**UPDATED**

In accordance with your authorization, Cobalt Geosciences, LLC has prepared a plan review letter for the project. We have included comments and responses from the September 19, 2025 City of Mercer Island letter. These are as follows:

There are comments regarding structural design and how it relates to potential lateral spread, ground loss, and structural deformation.

As noted in this letter, we estimated lateral spread of about 6 inches for the design event. We re-analyzed lateral spread with varying values for the grain size, thickness of saturated soils and fines content. This is discussed in more detail on Page 3.

Based on these results, lateral spread is most likely to occur near the eastern margin of the residential structure, decreasing to the west and generally increasing to the east.

We discussed potential use of grade beams to resist or manage these movements. It is our opinion that interconnecting grade beam systems embedded 2 to 3 feet below grade and supported on piles is a suitable option to limit lateral issues to an acceptable level. It may be necessary to space grade beams at 10 or 15 feet on center in east-west and north-south directions through the structure and backfill between the grade beams with compacted structural fill. Triangular grade beam layouts are known to be useful in liquefiable or lateral spread susceptible areas.

It is our opinion that slope stability analyses under seismic conditions are not warranted based on the soil composition/layering and low magnitude slopes in this area. The thickness of liquefiable soils in the CPT boring close to the house is minimal. The mat foundation is suitable to withstand the anticipated and analyzed lateral spread. The use of pin piles further reduces the risk of vertical settlement during or after seismic events.

**Plan Review:**

We have reviewed the architectural plans by MacPherson Construction and Design dated September 9, 2025, civil plans by Ethos Civil dated September 2, 2025, and structural plans by Mulhern Kulp dated October 22, 2024 and updated September 30, 2025. The plans appear to include relevant information from the geotechnical report. We have no comments at this time.

The following is the City-requested information regarding an updated statement of risk and discussion of subsurface soils and liquefaction hazards/mitigation from their letter dated August 27, 2025.

## Statement of Risk

Per Section 19.07.160B3 of the Mercer Island City Code, development within geologic hazard areas require that a Geotechnical Engineer licensed within the State of Washington provide a statement of risk with supporting documentation indicating that one of the following conditions can be met:

- a. The geologic hazard area will be modified, or the development has been designed so that the risk to the lot and adjacent property is eliminated or mitigated such that the site is determined to be safe; or
- b. An evaluation of site specific subsurface conditions demonstrates that the proposed development is not located in a geologic hazard area; or
- c. Development practices are proposed for the alteration that would render the development as safe as if it were not located in a geologic hazard area; or
- d. The alteration is so minor as not to pose a threat to the public health, safety and welfare.

The project meets the criteria of C from above. The construction will render the affected area as safe as if it were not located in a geologic hazard area. This includes deep foundation elements to support new foundations. The risk of landslide activity is low and will not be increased or decreased.

## CPT Boring and Liquefaction

The risk and amount of differential settlement between current auger-cast pile foundations and new pin pile supported foundation systems would be less than 1/2 inch over a 20 foot span. This of course relies on proper design and placement of both types of systems (older and upcoming). Pin piles driven to refusal typically experience very little post-construction settlement. Load testing to 200 percent of the design load commonly indicate less than 0.25 inches of movement. The risk of movements between the two types of foundation is low if piles are driven to refusal and existing foundations are confirmed through as built information (auger cast or piers).

Downdrag is not a common discussion or risk with piles smaller than about 6 inches in diameter. Larger piles are more likely to develop skin friction that could result in marginal to significant downdrag. It is our opinion that the risk of downdrag is low and does not pose a life safety risk. Mitigation is not warranted.

We recently advanced a Cone Penetrometer Test boring (CPT) in the driveway at the site. This log is attached with seismic information and soil behavior. To summarize, the boring encountered areas of fine grained soils within the upper 12.5 feet which were locally loose. Minor interbeds of these soils were present near 20 and 23 feet below grade. All other soils were mostly coarse grained with gravels and became consistently dense about 12.5 feet below grade. Very dense soils were encountered consistently below 34 feet with refusal.

We used the CPT information along with groundwater data from our previous boring to perform liquefaction analyses, which are attached. The analyses indicate up to 8.5 inches of total settlement due to liquefaction with differential settlement of about 4.25 inches over a span of 20 feet. We note that these analyses were likely conservative with lower average soil density for the units. The liquefaction zone was primarily 4 to 20 feet below grade.

The seismic testing/analysis indicates that Site Class E is present from about 0 to 20 feet below grade, Site Class D from 20 to 35 feet below grade, and Site Class C at 35 feet and below. Pin piles will likely achieve refusal in the coarse grained deposits between about 20 and 30 feet below grade. Site Class D appears to be reasonable. We recommend piles extending into dense soils at least 5 feet to refusal.

We analyzed the risk of lateral spread by the Bartlett and Youd method (1993). We determined a 1.45 kilometer distance between the site and Seattle Fault Zone from the DNR boring database and relevant thickness of soils with an N value of 15 or less (average), grain size, and slope between the property and Lake Washington.

The analyses yield an estimated 0.15 meters of lateral spread. This is about 6 inches of lateral movement. A mat foundation systems including interconnecting grade beams supported by pin piles could be utilized to resist lateral spread, if required. Battered piles may be an option but could result in some structural distress of the residence during/after certain seismic events.

We reanalyzed lateral spread with different values of T<sub>15</sub>, F<sub>15</sub> and D<sub>50-15</sub> to determine potential worse case and best case lateral spread displacement. We note that the displacements ranged from 4 to 18 inches in the area of Boring B-1, relatively close to Lake Washington. Displacements from the interpreted soil conditions in the CPT boring yielded values of 2 to 9 inches of displacement. The displacements are more limited due to minimal sand thicknesses. It is our opinion that the grade beam system supported on pipe piles are suitable for the site and lateral spread displacements will not result in structural damage that threatens life safety.

We must be on site to observe pile placement and other aspects of earthwork construction as noted in the previous geotechnical report and letters.

### **Mitigation Sequencing (Liquefaction)**

Discussion of mitigation sequencing is as follows:

Except as otherwise provided in this chapter, an applicant for a development proposal or activity shall implement the following sequential measures, listed below in order of preference, to avoid, minimize, and mitigate impacts to environmentally critical areas and associated buffers. Applicants shall document how each measure has been addressed before considering and incorporating the next measure in the sequence:

A. Avoiding the impact altogether by not taking a certain action or parts of an action. The applicant shall consider reasonable, affirmative steps and make best efforts to avoid critical area impacts. However, avoidance shall not be construed to mean mandatory withdrawal or denial of the development proposal or activity if the proposal or activity is an allowed, permitted, or conditional use in this title. In determining the extent to which the proposal should be redesigned to avoid the impact, the code official may consider the purpose, effectiveness, engineering feasibility, commercial availability of technology, best management practices, safety and cost of the proposal and identified changes to the proposal. Development proposals should seek to avoid, minimize and mitigate overall impacts based on the functions and values of all of the relevant critical areas and based on the recommendations of a critical area study. If impacts cannot be avoided through redesign, use of a setback deviation pursuant to section [19.06.110\(C\)](#), or because of site conditions or project requirements, the applicant shall then proceed with the sequence of steps in subsections B through E of this section;

We have analyzed liquefaction risks and provided recommendations for deep foundations, similar to what is currently present. Mitigation of liquefaction risks was not avoidable due to the geologic conditions.

B. Minimizing impacts by limiting the degree or magnitude of the action and its implementation, using a setback deviation pursuant to section [19.06.110\(C\)](#), using appropriate technology, or by taking affirmative steps to avoid or reduce impacts;

Pile installation with grade beams is the least impactful method to create a stable building pad and foundation system.

C. Rectifying the impact by repairing, rehabilitating, or restoring the affected environment;

Not applicable. Piles reduce the impact by transferring building loads to deeper bearing strata.

D. Reducing or eliminating the impact over time by preservation and maintenance operations during the life of the action;

Not applicable.

E. Compensating for the impact by replacing, enhancing, or providing substitute resources or environments; and/or

Not applicable.

F. Monitoring the impact and taking appropriate corrective measures to maintain the integrity of compensating measures.

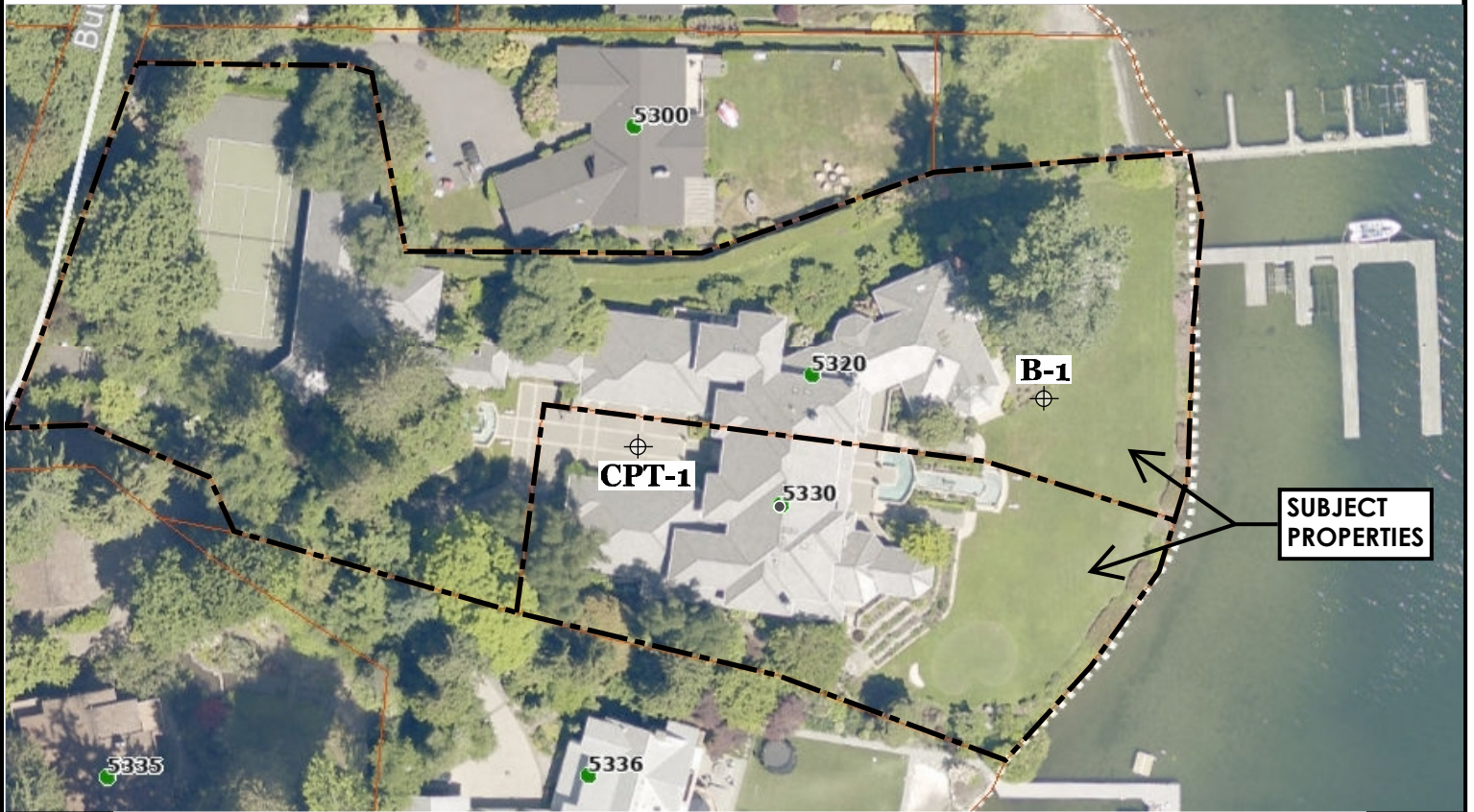
Monitoring would include observation of pile installation and load testing. Post construction monitoring is not required.

Sincerely,

**Cobalt Geosciences, LLC**



10/21/2025  
Phil Haberman, PE, LG, LEG  
Princip



**B-1**  
**CPT-1**



**Approximate  
Boring and CPT Boring Locations**



Not to Scale



Proposed Remodel  
5320 and 5330 Butterworth Road  
Mercer Island, Washington

**SITE MAP**  
**FIGURE 1**

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## Unified Soil Classification System (USCS)

MAJOR DIVISIONS			SYMBOL	TYPICAL DESCRIPTION	
<b>COARSE GRAINED SOILS</b> (more than 50% retained on No. 200 sieve)	Gravels (more than 50% of coarse fraction retained on No. 4 sieve)	Clean Gravels (less than 5% fines)	GW	Well-graded gravels, gravels, gravel-sand mixtures, little or no fines	
		Gravels with Fines (more than 12% fines)	GP	Poorly graded gravels, gravel-sand mixtures, little or no fines	
		Sands (50% or more of coarse fraction passes the No. 4 sieve)	Clean Sands (less than 5% fines)	GM	Silty gravels, gravel-sand-silt mixtures
			Sands with Fines (more than 12% fines)	GC	Clayey gravels, gravel-sand-clay mixtures
	<b>FINE GRAINED SOILS</b> (50% or more passes the No. 200 sieve)	Silts and Clays (liquid limit less than 50)	Inorganic	ML	Inorganic silts of low to medium plasticity, sandy silts, gravelly silts, or clayey silts with slight plasticity
			Organic	OL	Organic silts and organic silty clays of low plasticity
			Silts and Clays (liquid limit 50 or more)	Inorganic	MH
		Organic		CH	Inorganic clays of medium to high plasticity, sandy fat clay, or gravelly fat clay
		Organic		OH	Organic clays of medium to high plasticity, organic silts
		Inorganic	CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy silty clays, lean clays	
Organic	SM	Silty sands, sand-silt mixtures			
Organic	SC	Clayey sands, sand-clay mixtures			
Organic	SP	Poorly graded sand, gravelly sands, little or no fines			
Organic	SW	Well-graded sands, gravelly sands, little or no fines			
Organic	PT	Peat, humus, swamp soils with high organic content (ASTM D4427)			
<b>HIGHLY ORGANIC SOILS</b>	Primarily organic matter, dark in color, and organic odor		PT	Peat, humus, swamp soils with high organic content (ASTM D4427)	

Classification of Soil Constituents
<p>MAJOR constituents compose more than 50 percent, by weight, of the soil. Major constituents are capitalized (i.e., SAND).</p> <p>Minor constituents compose 12 to 50 percent of the soil and precede the major constituents (i.e., silty SAND). Minor constituents preceded by "slightly" compose 5 to 12 percent of the soil (i.e., slightly silty SAND).</p> <p>Trace constituents compose 0 to 5 percent of the soil (i.e., slightly silty SAND, trace gravel).</p>

Grain Size Definitions	
Description	Sieve Number and/or Size
Fines	< #200 (0.08 mm)
Sand	#200 to #40 (0.08 to 0.4 mm)
-Fine	#40 to #10 (0.4 to 2 mm)
-Medium	#10 to #4 (2 to 5 mm)
-Coarse	
Gravel	#4 to 3/4 inch (5 to 19 mm)
-Fine	3/4 to 3 inches (19 to 76 mm)
-Coarse	
Cobbles	3 to 12 inches (75 to 305 mm)
Boulders	>12 inches (305 mm)

Relative Density (Coarse Grained Soils)		Consistency (Fine Grained Soils)	
N, SPT, Blows/FT	Relative Density	N, SPT, Blows/FT	Relative Consistency
0 - 4	Very loose	Under 2	Very soft
4 - 10	Loose	2 - 4	Soft
10 - 30	Medium dense	4 - 8	Medium stiff
30 - 50	Dense	8 - 15	Stiff
Over 50	Very dense	15 - 30	Very stiff
		Over 30	Hard

Moisture Content Definitions	
Dry	Absence of moisture, dusty, dry to the touch
Moist	Damp but no visible water
Wet	Visible free water, from below water table



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Soil Classification Chart

Figure C1

# Log of Boring B-1

Date: May 15, 2024	Depth: 16.5'	Initial Groundwater: 4'
Contractor: CN	Elevation:	Sample Type: Split Spoon
Method: Hollow Stem Auger	Logged By: PH    Checked By: SC	Final Groundwater: 4'

Depth (Feet)	Interval	% Recovery	Blows/6"	Graphic Log	USCS Symbol	Material Description	Groundwater	Moisture Content (%)	
								Plastic Limit	Liquid Limit
								SPT N-Value	
								0	50
				Vegetation/Topsoil					
0			0		SM	Very loose to loose, silty-fine to medium grained sand, dark yellowish brown, moist to wet. (Fill)	0		
2			1						
4			1						
6			2		SP	Loose to medium dense, fine to medium grained sand, mottled olive gray, moist to wet. (Pre-Olympia Deposits)	5		
8			1						
10			3						
12			4						
14			10						
16			2						
16			3						
16			2						
18						End of Boring 16.5' Refusal due to heave.			
20									
22									
24									
26									
28									
30									
32									
34									



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Proposed Residence  
 5330 Butterworth Road  
 Mercer Island, Washington

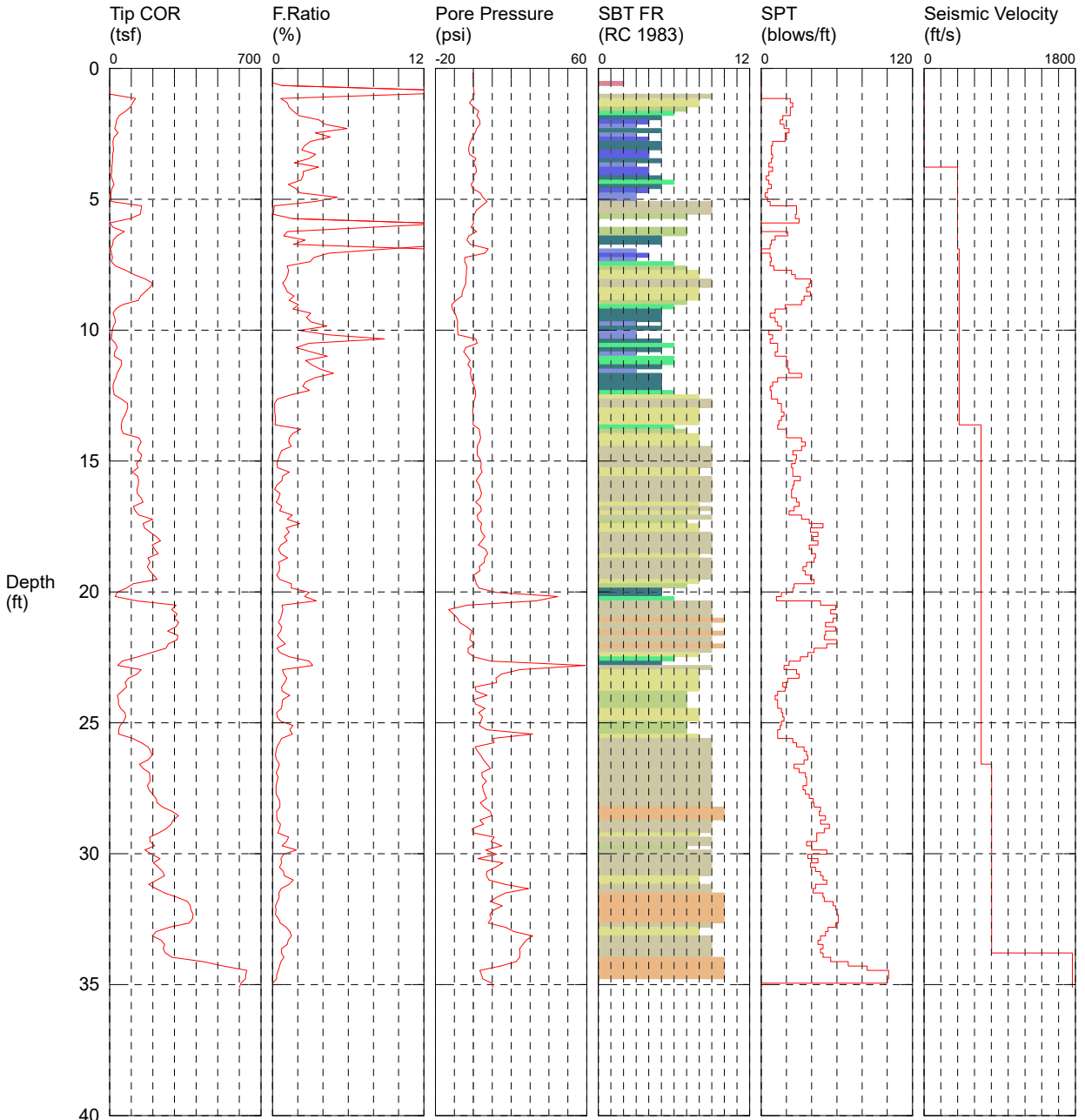
**Boring  
 Log**



# sCPT-01

CPT Contractor: In Situ Engineering  
 CUSTOMER: Cobalt Geo  
 LOCATION: Mercer Isd  
 JOB NUMBER:  
 COMMENT: Butterworth

OPERATOR: Okbay  
 CONE ID: DDG1351  
 TEST DATE: 11/19/2024 10:29:18 AM  
 PREDRILL: 1 ft  
 BACKFILL: 20% Bentonite slurry & Chips  
 SURFACE PATCH: Concrete Patch

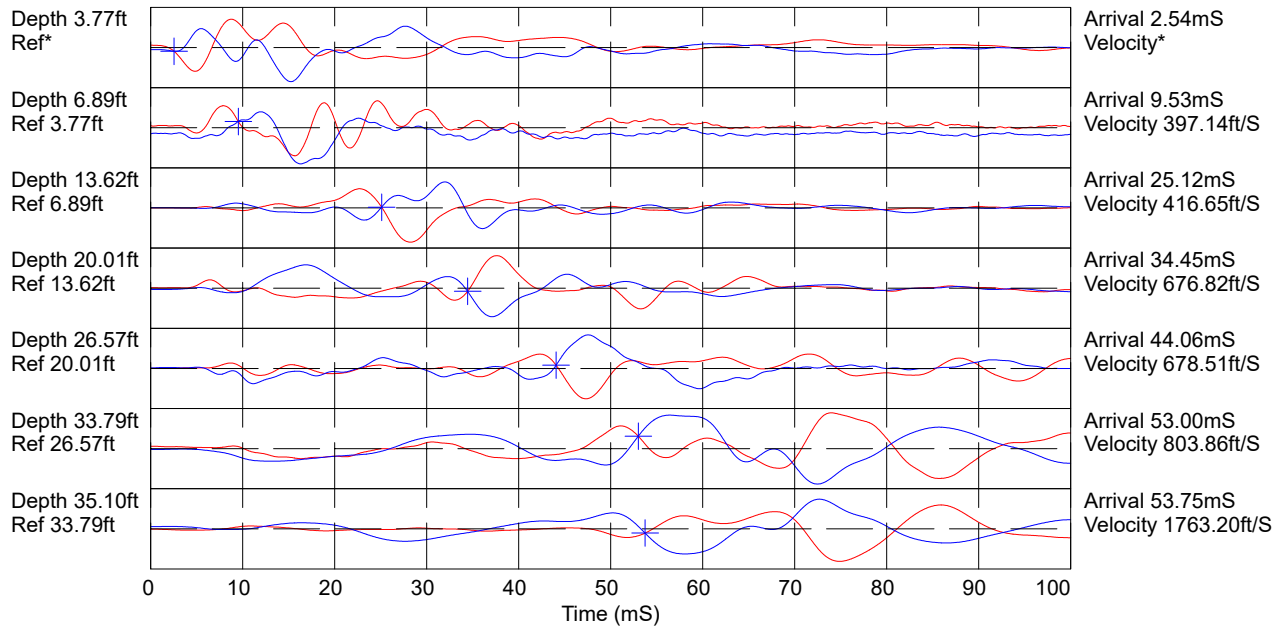


TOTAL DEPTH: 35.105 ft

- |                          |                             |                            |                                |
|--------------------------|-----------------------------|----------------------------|--------------------------------|
| 1 sensitive fine grained | 4 silty clay to clay        | 7 silty sand to sandy silt | 10 gravelly sand to sand       |
| 2 organic material       | 5 clayey silt to silty clay | 8 sand to silty sand       | 11 very stiff fine grained (*) |
| 3 clay                   | 6 sandy silt to clayey silt | 9 sand                     | 12 sand to clayey sand (*)     |

\*SBT/SPT CORRELATION: UBC-1983

HOLE NUMBER: sCPT-01



Hammer to Rod String Distance (ft): 2.62  
\* = Not Determined

**SPT BASED LIQUEFACTION ANALYSIS REPORT**

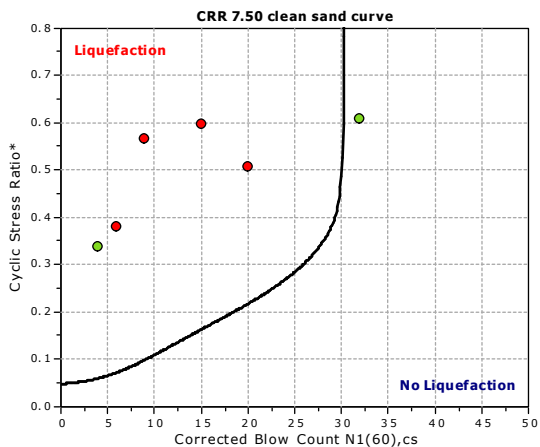
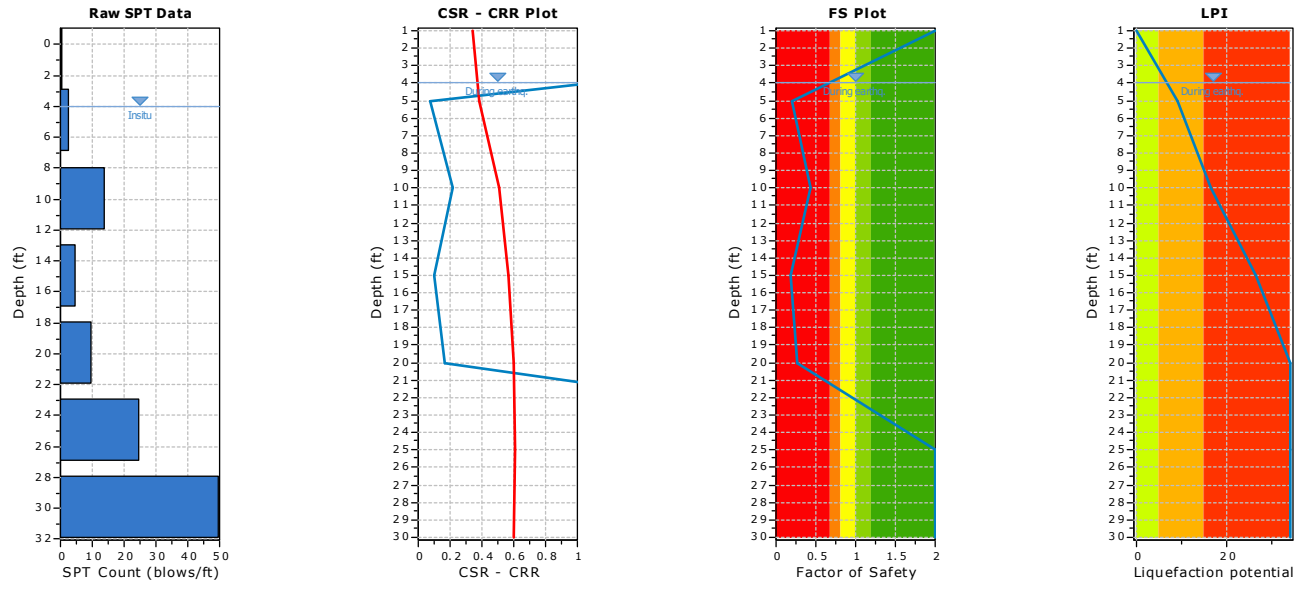
**Project title : Butterworth**

**SPT Name: SPT #1**

**Location : Mercer Island**

**:: Input parameters and analysis properties ::**

Analysis method:	NCEER 1998	G.W.T. (in-situ):	4.00 ft
Fines correction method:	NCEER 1998	G.W.T. (earthq.):	4.00 ft
Sampling method:	Standard Sampler	Earthquake magnitude $M_w$ :	7.00
Borehole diameter:	65mm to 115mm	Peak ground acceleration:	0.62 g
Rod length:	3.30 ft	Eq. external load:	0.00 tsf
Hammer energy ratio:	1.00		



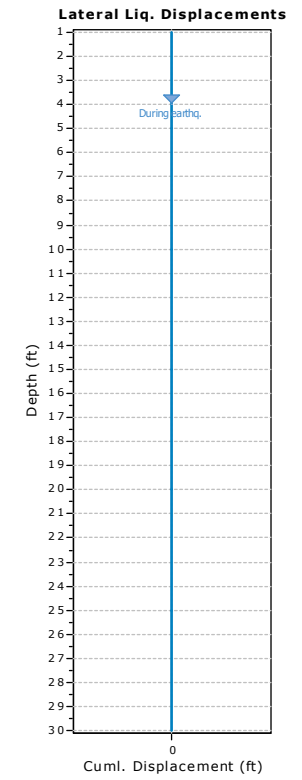
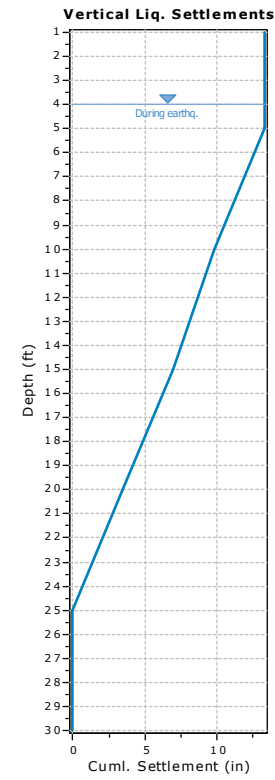
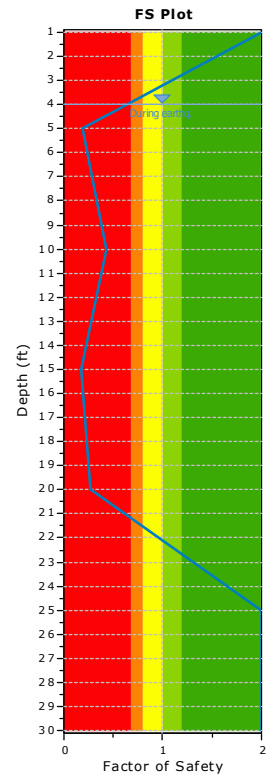
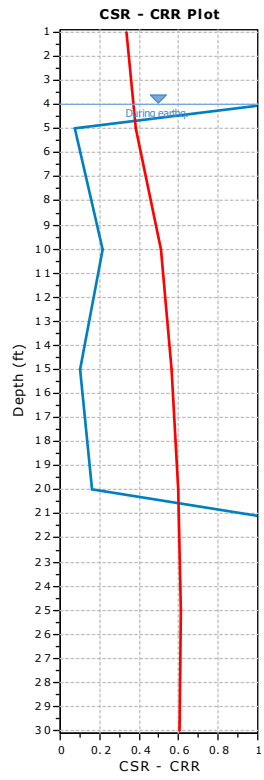
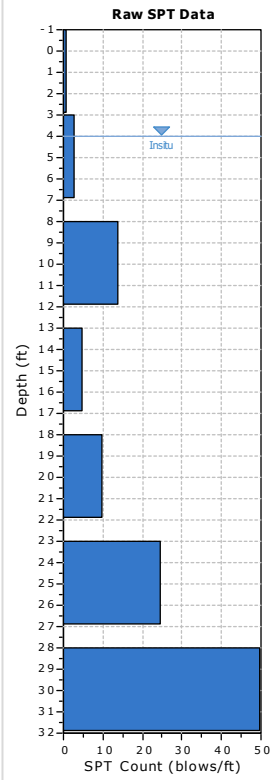
**F.S. color scheme**

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

**LPI color scheme**

- Very high risk
- High risk
- Low risk

**:: Overall Liquefaction Assessment Analysis Plots ::**



:: Field input data ::					
Test Depth (ft)	SPT Field Value (blows)	Fines Content (%)	Unit Weight (pcf)	Infl. Thickness (ft)	Can Liquefy
1.00	1	15.00	105.00	4.00	Yes
5.00	3	15.00	105.00	5.00	Yes
10.00	14	15.00	110.00	5.00	Yes
15.00	5	15.00	110.00	5.00	Yes
20.00	10	15.00	110.00	5.00	Yes
25.00	25	15.00	115.00	5.00	Yes
30.00	50	25.00	120.00	5.00	No

**Abbreviations**

Depth: Depth at which test was performed (ft)  
 SPT Field Value: Number of blows per foot  
 Fines Content: Fines content at test depth (%)  
 Unit Weight: Unit weight at test depth (pcf)  
 Infl. Thickness: Thickness of the soil layer to be considered in settlements analysis (ft)  
 Can Liquefy: User defined switch for excluding/including test depth from the analysis procedure

:: Cyclic Resistance Ratio (CRR) calculation data ::																
Depth (ft)	SPT Field Value	Unit Weight (pcf)	$\sigma_v$ (tsf)	$u_o$ (tsf)	$\sigma'_{vo}$ (tsf)	$C_N$	$C_E$	$C_B$	$C_R$	$C_S$	$(N_1)_{60}$	Fines Content (%)	$\alpha$	$\beta$	$(N_1)_{60cs}$	CRR <sub>7.5</sub>
1.00	1	105.00	0.05	0.00	0.05	1.70	1.00	1.00	0.75	1.00	1	15.00	2.50	1.05	4	4.000
5.00	3	105.00	0.26	0.03	0.23	1.55	1.00	1.00	0.75	1.00	3	15.00	2.50	1.05	6	0.073
10.00	14	110.00	0.54	0.19	0.35	1.44	1.00	1.00	0.85	1.00	17	15.00	2.50	1.05	20	0.218
15.00	5	110.00	0.81	0.34	0.47	1.34	1.00	1.00	0.85	1.00	6	15.00	2.50	1.05	9	0.099
20.00	10	110.00	1.09	0.50	0.59	1.25	1.00	1.00	0.95	1.00	12	15.00	2.50	1.05	15	0.163
25.00	25	115.00	1.38	0.66	0.72	1.17	1.00	1.00	0.95	1.00	28	15.00	2.50	1.05	32	4.000
30.00	50	120.00	1.68	0.81	0.86	1.09	1.00	1.00	1.00	1.00	55	25.00	4.29	1.11	66	4.000

**Abbreviations**

$\sigma_v$ : Total stress during SPT test (tsf)  
 $u_o$ : Water pore pressure during SPT test (tsf)  
 $\sigma'_{vo}$ : Effective overburden pressure during SPT test (tsf)  
 $C_N$ : Overburden correction factor  
 $C_E$ : Energy correction factor  
 $C_B$ : Borehole diameter correction factor  
 $C_R$ : Rod length correction factor  
 $C_S$ : Liner correction factor  
 $N_{1(60)}$ : Corrected  $N_{SPT}$  to a 60% energy ratio  
 $\alpha, \beta$ : Clean sand equivalent clean sand formula coefficients  
 $N_{1(60)cs}$ : Corrected  $N_{1(60)}$  value for fines content  
 CRR<sub>7.5</sub>: Cyclic resistance ratio for M=7.5

:: Cyclic Stress Ratio calculation (CSR fully adjusted and normalized) ::													
Depth (ft)	Unit Weight (pcf)	$\sigma_{v,eq}$ (tsf)	$u_{o,eq}$ (tsf)	$\sigma'_{vo,eq}$ (tsf)	$r_d$	$\alpha$	CSR	MSF	CSR <sub>eq, M=7.5</sub>	$K_{\sigma gma}$	CSR*	FS	
1.00	105.00	0.05	0.00	0.05	1.00	1.00	0.403	1.19	0.338	1.00	0.338	2.000	●
5.00	105.00	0.26	0.03	0.23	0.99	1.00	0.453	1.19	0.380	1.00	0.380	0.192	●
10.00	110.00	0.54	0.19	0.35	0.98	1.00	0.605	1.19	0.508	1.00	0.508	0.429	●
15.00	110.00	0.81	0.34	0.47	0.97	1.00	0.676	1.19	0.567	1.00	0.567	0.175	●
20.00	110.00	1.09	0.50	0.59	0.96	1.00	0.713	1.19	0.598	1.00	0.598	0.273	●
25.00	115.00	1.38	0.66	0.72	0.94	1.00	0.725	1.19	0.608	1.00	0.608	2.000	●
30.00	120.00	1.68	0.81	0.86	0.92	1.00	0.719	1.19	0.603	1.00	0.603	2.000	●

:: Cyclic Stress Ratio calculation (CSR fully adjusted and normalized) ::												
Depth (ft)	Unit Weight (pcf)	$\sigma_{v,eq}$ (tsf)	$u_{o,eq}$ (tsf)	$\sigma'_{vo,eq}$ (tsf)	$r_d$	$\alpha$	CSR	MSF	$CSR_{eq,M=7.5}$	$K_{\sigma_{\text{sigma}}}$	CSR*	FS

**Abbreviations**

- $\sigma_{v,eq}$ : Total overburden pressure at test point, during earthquake (tsf)
- $u_{o,eq}$ : Water pressure at test point, during earthquake (tsf)
- $\sigma'_{vo,eq}$ : Effective overburden pressure, during earthquake (tsf)
- $r_d$ : Nonlinear shear mass factor
- $\alpha$ : Improvement factor due to stone columns
- CSR: Cyclic Stress Ratio (adjusted for improvement)
- MSF: Magnitude Scaling Factor
- $CSR_{eq,M=7.5}$ : CSR adjusted for M=7.5
- $K_{\sigma_{\text{sigma}}}$ : Effective overburden stress factor
- CSR\*: CSR fully adjusted (user FS applied)\*\*\*
- FS: Calculated factor of safety against soil liquefaction

\*\*\* User FS: 1.00

:: Liquefaction potential according to Iwasaki ::					
Depth (ft)	FS	F	wz	Thickness (ft)	$I_L$
1.00	2.000	0.00	9.85	4.00	0.00
5.00	0.192	0.81	9.24	4.00	9.10
10.00	0.429	0.57	8.48	5.00	7.38
15.00	0.175	0.82	7.71	5.00	9.70
20.00	0.273	0.73	6.95	5.00	7.70
25.00	2.000	0.00	6.19	5.00	0.00
30.00	2.000	0.00	5.43	5.00	0.00

**Overall potential  $I_L$ : 33.87**

- $I_L = 0.00$  - No liquefaction
- $I_L$  between 0.00 and 5 - Liquefaction not probable
- $I_L$  between 5 and 15 - Liquefaction probable
- $I_L > 15$  - Liquefaction certain

:: Vertical settlements estimation for dry sands ::												
Depth (ft)	$(N_1)_{60}$	$\tau_{av}$	p	$G_{max}$ (tsf)	$\alpha$	b	$\gamma$	$\epsilon_{15}$	$N_c$	$\epsilon_{N_c}$ (%)	$\Delta h$ (ft)	$\Delta S$ (in)
1.00	1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	4.00	0.000

**Cumulative settlements: 0.000**

**Abbreviations**

- $\tau_{av}$ : Average cyclic shear stress
- p: Average stress
- $G_{max}$ : Maximum shear modulus (tsf)
- $\alpha, b$ : Shear strain formula variables
- $\gamma$ : Average shear strain
- $\epsilon_{15}$ : Volumetric strain after 15 cycles
- $N_c$ : Number of cycles
- $\epsilon_{N_c}$ : Volumetric strain for number of cycles  $N_c$  (%)
- $\Delta h$ : Thickness of soil layer (in)
- $\Delta S$ : Settlement of soil layer (in)

:: Vertical settlements estimation for saturated sands ::					
Depth (ft)	$D_{50}$ (in)	$q_c/N$	$e_v$ (%)	$\Delta h$ (ft)	s (in)

<b>:: Vertical settlements estimation for saturated sands ::</b>					
<b>Depth (ft)</b>	<b>D<sub>50</sub> (in)</b>	<b>q<sub>c</sub>/N</b>	<b>e<sub>v</sub> (%)</b>	<b>Δh (ft)</b>	<b>s (in)</b>
5.00	0.01	2.10	5.80	5.00	3.480
10.00	0.01	2.10	4.76	5.00	2.853
15.00	0.01	2.10	5.80	5.00	3.480
20.00	0.01	2.10	5.80	5.00	3.480
25.00	0.01	2.10	0.00	5.00	0.000
30.00	0.01	2.10	0.00	5.00	0.000

**Cumulative settlements: 13.293**

**Abbreviations**

- D<sub>50</sub>: Median grain size (in)
- q<sub>c</sub>/N: Ratio of cone resistance to SPT
- e<sub>v</sub>: Post liquefaction volumetric strain (%)
- Δh: Thickness of soil layer to be considered (ft)
- s: Estimated settlement (in)

<b>:: Lateral displacements estimation for saturated sands ::</b>						
<b>Depth (ft)</b>	<b>(N<sub>1</sub>)<sub>60</sub></b>	<b>D<sub>r</sub> (%)</b>	<b>γ<sub>max</sub> (%)</b>	<b>d<sub>z</sub> (ft)</b>	<b>LDI</b>	<b>LD (ft)</b>
1.00	1	14.00	0.00	4.00	0.000	0.00
5.00	3	24.25	51.20	5.00	0.000	0.00
10.00	17	57.72	22.70	5.00	0.000	0.00
15.00	6	34.29	51.20	5.00	0.000	0.00
20.00	12	48.50	34.10	5.00	0.000	0.00
25.00	28	74.08	0.00	5.00	0.000	0.00
30.00	55	100.00	0.00	5.00	0.000	0.00

**Cumulative lateral displacements: 0.00**

**Abbreviations**

- D<sub>r</sub>: Relative density (%)
- γ<sub>max</sub>: Maximum amplitude of cyclic shear strain (%)
- d<sub>z</sub>: Soil layer thickness (ft)
- LDI: Lateral displacement index (ft)
- LD: Actual estimated displacement (ft)

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